





EM-based Design Optimization of RF and Microwave Circuits using Functional Surrogate Models

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presented at Workshop on Simulation- and Surrogate-Driven Microwave Design Technology (WME) IEEE MTT-S International Microwave Symposium, Baltimore, MD, June 6, 2011





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Abstract

An effective CAD methodology to perform efficient EM-based design optimization of microwave circuits using surrogate models based on polynomial functional interpolants is described. This surrogate-driven design procedure is especially suitable for cases where a continuous coarse model is not available. The corresponding surrogate models are formulated as low-order functions of the design variables, and are used to interpolate highly accurate electromagnetic responses in a region of interest around a selected reference design. Global optimal values for the surrogate model weighting factors are efficiently obtained in closed form, using compact formulas. Exhaustive evaluation of the generalization performance of this surrogate modeling approach is addressed. The proposed CAD methodology is illustrated using commercially available EM simulators Sonnet and CST Microwave Studio for the design optimization of several high-speed PCB interconnect structures.





Outline

- Surrogate modeling
- Surrogate modeling using polynomial interpolants
- Generalization performance of polynomial surrogates
- Surrogate-driven optimization of an SIW-CPW transition
- Surrogate-driven optimization of microstrip traces with via fences
- Conclusions

Surrogate Modeling

- Design optimization of microwave circuits requires accurate and inexpensive models
- Surrogate models were proposed for efficient and accurate optimization of expensive functions (fine models)
- Surrogate modeling refers to the iterative construction of functional relationships based on a limited amount of fine model data with no derivatives information







Surrogate Modeling using Polynomials

- It takes as a basis a "zero-order" model:
 - Fixed fine model response, or
 - Input-mapped coarse model
- Multidimensional polynomials enhance the zero-order model around a reference design
- Closed-form expression are used to calculate the functional weighting factors (globally optimal)
- It uses a limited amount fine model data

Fine, Coarse and Surrogate Models

- *R*_f ∈ ℜ^p: fine model response sampled at *p* independent-variable points; evaluating *R*_f(*x*) is expensive
- $x \in \Re^n$: design variables
- *R*_c ∈ ℜ^p : coarse model response; evaluating *R*_c(*x*) is inexpensive
- We want a surrogate model $\mathbf{R}_{s}(\mathbf{x}) : X_{s} \to \Re^{p}$ such that $\mathbf{R}_{s}(\mathbf{x}) \approx \mathbf{R}_{f}(\mathbf{x})$ in a region X_{s} around $\mathbf{x}^{(0)}$
- To "train" the surrogate model, we use *L* learning points, denoted as x⁽¹⁾, x⁽²⁾, ..., x^(L)
- To test the surrogate model we use *T* testing points

(Bandler et al., 2000)







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"Zero-Order" Models

• Fixed fine model response

$$\boldsymbol{R}_{s}^{(0)}(\boldsymbol{x}) = \boldsymbol{R}_{f}(\boldsymbol{x}^{(0)}) \text{ for all } \boldsymbol{x} \in X_{s}$$

Linearly input mapped coarse model

$$\mathbf{R}_{s}^{(0)}(\mathbf{x}) = \mathbf{R}_{c}(\mathbf{B}\mathbf{x} + \mathbf{c})$$
 for all $\mathbf{x} \in X_{s}$

where $\boldsymbol{B} \in \Re^{n \times n}$ and $\boldsymbol{c} \in \Re^n$

 Linear input mapped coarse model with local output correction

$$\mathbf{R}_{s}^{(0)}(\mathbf{x}) = \mathbf{R}_{c}(\mathbf{B}\mathbf{x} + \mathbf{c}) + \mathbf{d}$$
 for all $\mathbf{x} \in X_{s}$

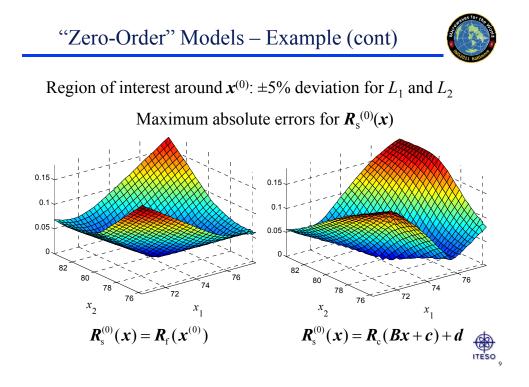
where $\boldsymbol{d} \in \Re^p$

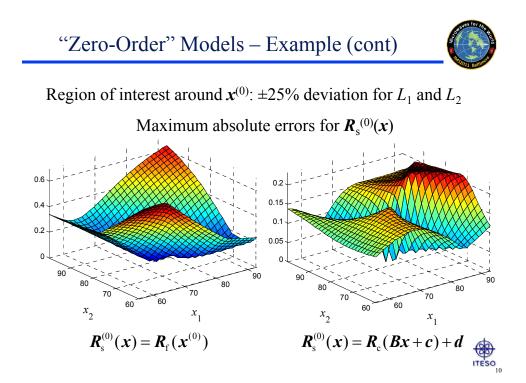
"Zero-Order" Models – Example Coarse Model $x = [L_1 \ L_2]^T$ (electrical lengths at 1GHz, in degrees) $\geq 10\Omega$ Z_1 Z_2 $\mathbf{x}^{(0)} = [74.14 \quad 79.64]^{\mathrm{T}}$ $\boldsymbol{R}_{f} \in \Re^{p}$ is $|S_{11}|$ for "Fine" Model 0.2GHz $\le f \le 1.8$ GHz, p = 300Two cases: $\boldsymbol{R}_{\mathrm{s}}^{(0)}(\boldsymbol{x}) = \boldsymbol{R}_{\mathrm{f}}(\boldsymbol{x}^{(0)})$ Z_2 Z_1 1ÕΩ $\boldsymbol{R}_{s}^{(0)}(\boldsymbol{x}) = \boldsymbol{R}_{c}(\boldsymbol{B}\boldsymbol{x} + \boldsymbol{c}) + \boldsymbol{d}$ (**B** and **c** obtained $C_1 = C_2 = C_3 = 10 \text{pF}$ after a BBSM) $Z_1 = 2.23615\Omega, Z_2 = 4.47230\Omega$





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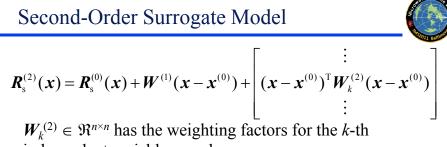
$$R_{s}^{(1)}(x) = R_{s}^{(0)}(x) + W^{(1)}(x - x^{(0)})$$
 for all $x \in X_{s}$

where $W^{(1)} \in \Re^{p \times n}$ contains all the weighting factors,

$$\boldsymbol{W}^{(1)} = \boldsymbol{\varDelta} \boldsymbol{R}^{(0)} (\boldsymbol{\varDelta} \boldsymbol{x}^{(1)})^{+}$$

where $(\cdot)^+$ denotes the pseudo-inverse, and $\Delta \mathbf{x}^{(1)} \in \Re^{n \times L}$ and $\Delta \mathbf{R}^{(0)} \in \Re^{p \times L}$ are

$$\boldsymbol{\Delta x}^{(1)} = \begin{bmatrix} (\boldsymbol{x}^{(1)} - \boldsymbol{x}^{(0)}) \\ (\boldsymbol{x}^{(2)} - \boldsymbol{x}^{(0)}) \\ \vdots \\ (\boldsymbol{x}^{(L)} - \boldsymbol{x}^{(0)}) \end{bmatrix}^{\mathrm{T}}, \ \boldsymbol{\Delta R}^{(0)} = \begin{bmatrix} \boldsymbol{R}_{\mathrm{f}}(\boldsymbol{x}^{(1)}) - \boldsymbol{R}_{\mathrm{s}}^{(0)}(\boldsymbol{x}^{(1)}) \\ \boldsymbol{R}_{\mathrm{f}}(\boldsymbol{x}^{(2)}) - \boldsymbol{R}_{\mathrm{s}}^{(0)}(\boldsymbol{x}^{(2)}) \\ \vdots \\ \boldsymbol{R}_{\mathrm{f}}(\boldsymbol{x}^{(L)}) - \boldsymbol{R}_{\mathrm{s}}^{(0)}(\boldsymbol{x}^{(L)}) \end{bmatrix}^{\mathrm{T}}$$



independent variable sample

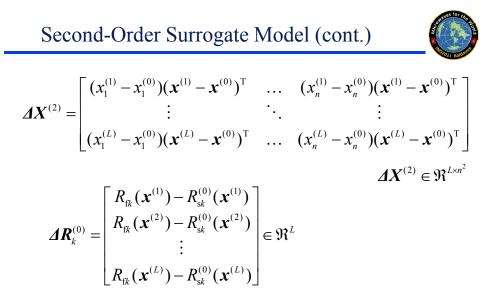
$$\boldsymbol{w}_k = (\boldsymbol{\Delta} \boldsymbol{X})^+ \boldsymbol{\Delta} \boldsymbol{R}_k^{(0)} \quad \text{for } k = 1 \dots p$$

where vector \boldsymbol{w}_k contains the rows of $\boldsymbol{W}^{(1)}$ and all the columns of $\boldsymbol{W}_k^{(2)}$,

$$\boldsymbol{w}_{k} = [\boldsymbol{w}_{k}^{(1)} \ \boldsymbol{w}_{k1}^{(2)} \ \boldsymbol{w}_{k2}^{(2)} \ \dots \ \boldsymbol{w}_{kn}^{(2)}]^{\mathrm{T}} \in \mathfrak{R}^{(n^{2}+n)}$$

and

 $\Delta \boldsymbol{X} = [\boldsymbol{\Delta x}^{(1)^{\mathrm{T}}} \quad \boldsymbol{\Delta X}^{(2)}] \in \mathfrak{R}^{L \times (n^{2} + n)}$



We have generalized this formulation for an *N*-th order surrogate model

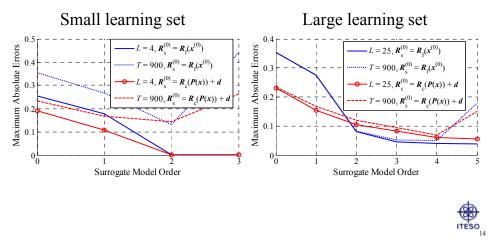


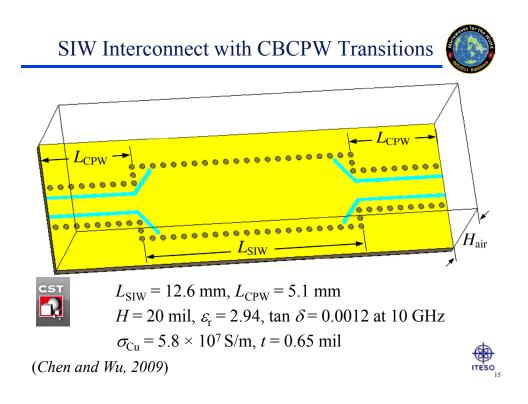
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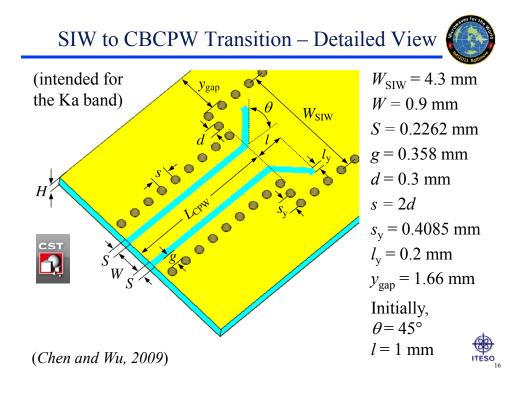
Impedance Transformer Example

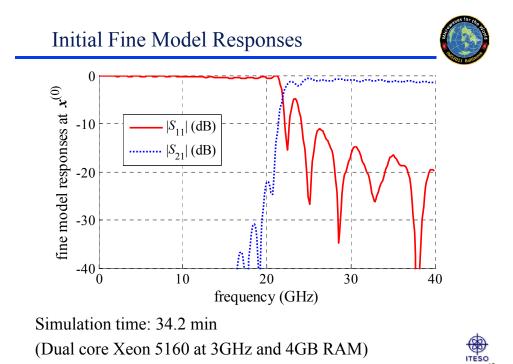
Errors in learning and testing sets for the surrogate models

Region of interest around $\mathbf{x}^{(0)}$: ±10% deviation for L_1 and L_2









Surrogate Model of the SIW-CBCPW

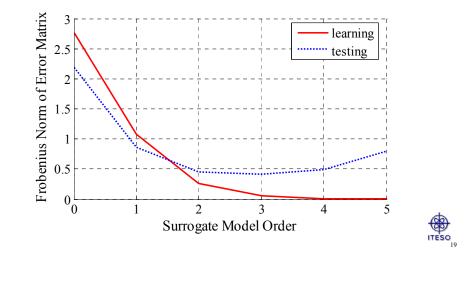


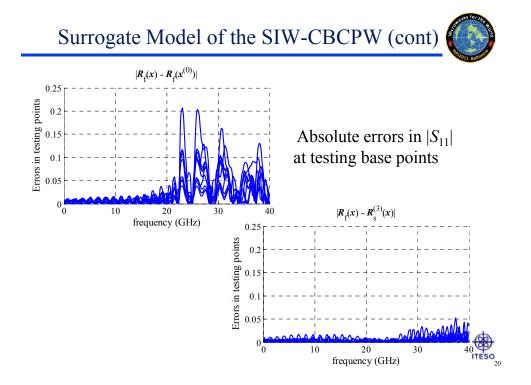
- We select $\mathbf{x} = [\theta (\text{degrees}) \ l(\text{mm})]^{\text{T}}$
- $x^{(0)} = [45 \ 1]^{\mathrm{T}}$
- $R_{\rm s}^{(0)}(x) = R_{\rm f}(x^{(0)})$
- Region of interest around x⁽⁰⁾: ±15% deviation for θ and ±5% deviation for l
- We use 8 learning base points
- We use 10 random test points

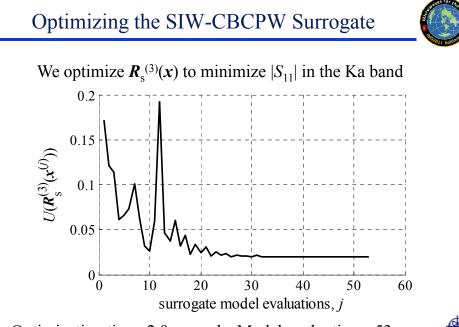




Errors in learning and testing sets for the surrogate models of $|S_{11}|$

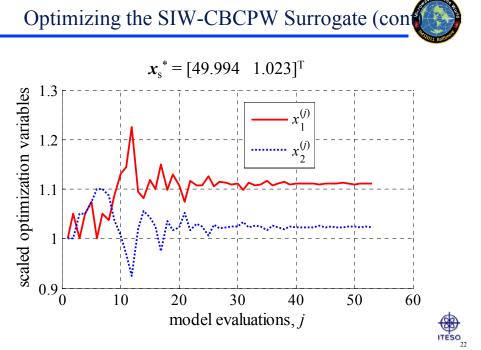


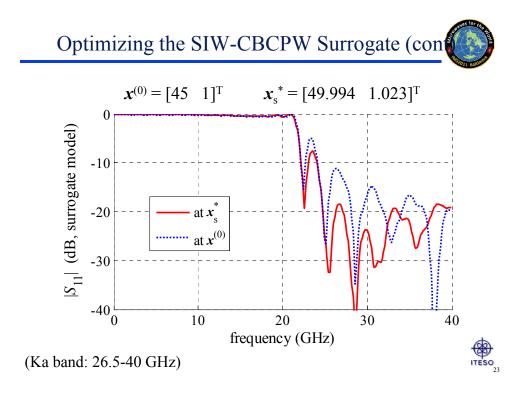


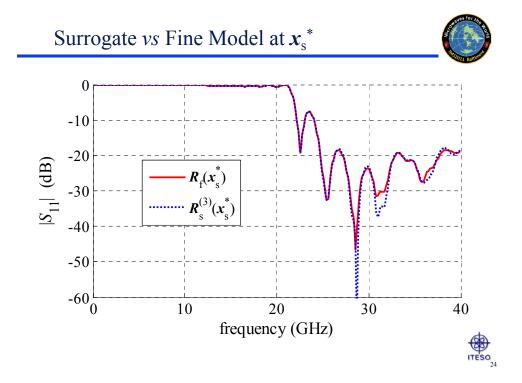


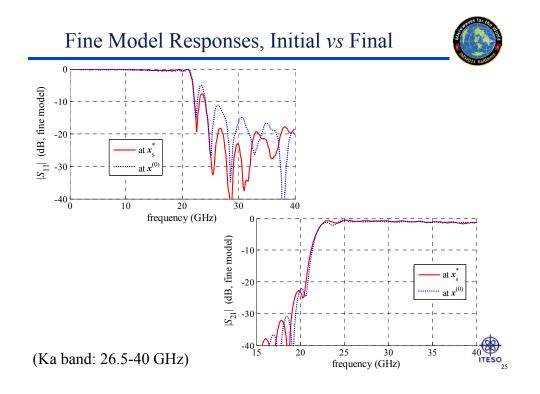
Optimization time: 2.9 seconds; Model evaluations: 53







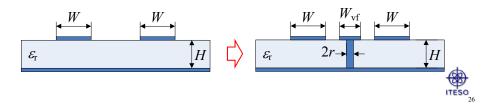


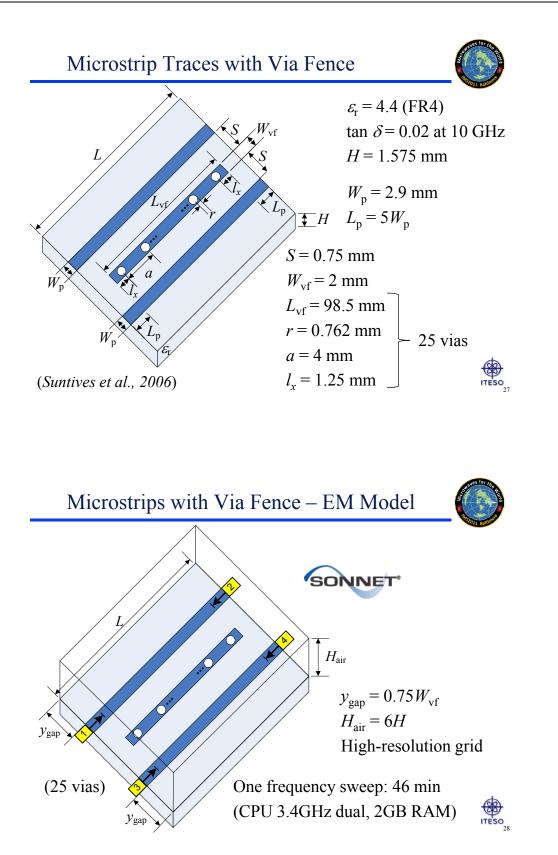


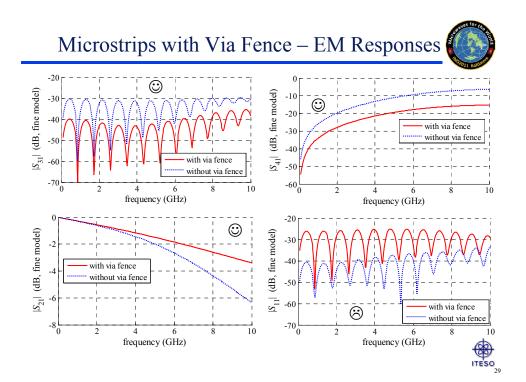
Crosstalk Reduction by Guard Traces

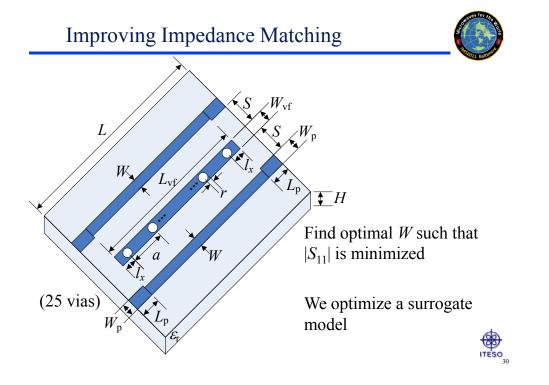


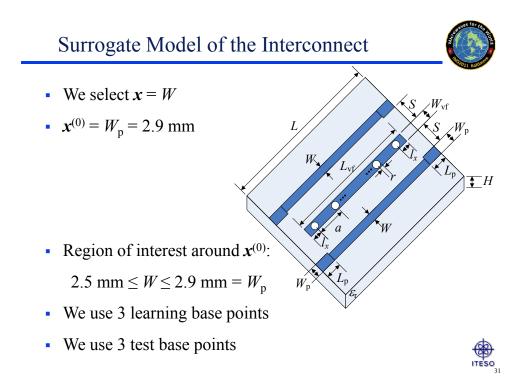
- Crosstalk is a major concern in high-speed interconnect design
- A traditional technique to minimize crosstalk consists of using via fences or guard traces
- Inserting via fences between microstrip lines effectively reduces crosstalk and transmission losses
- · However, via fences deteriorate impedance matching







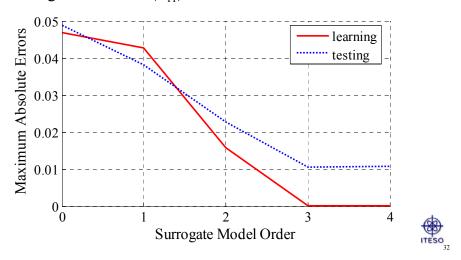


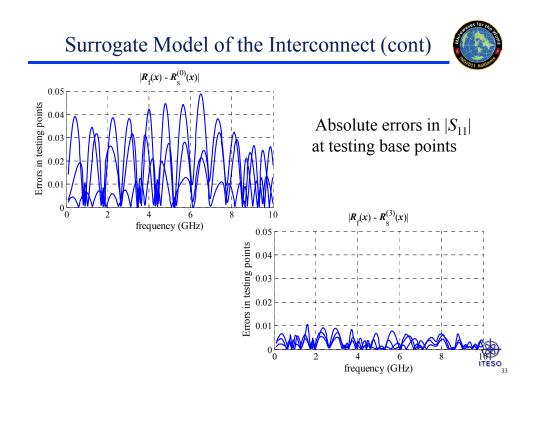


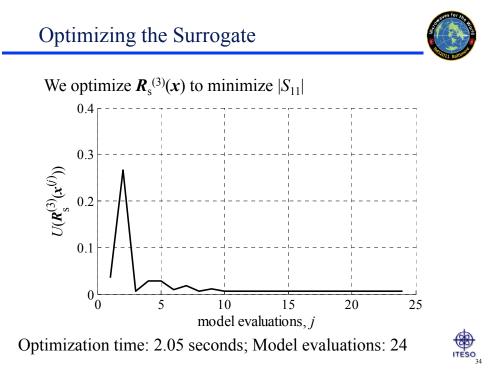
Surrogate Model of the Interconnect (cont)

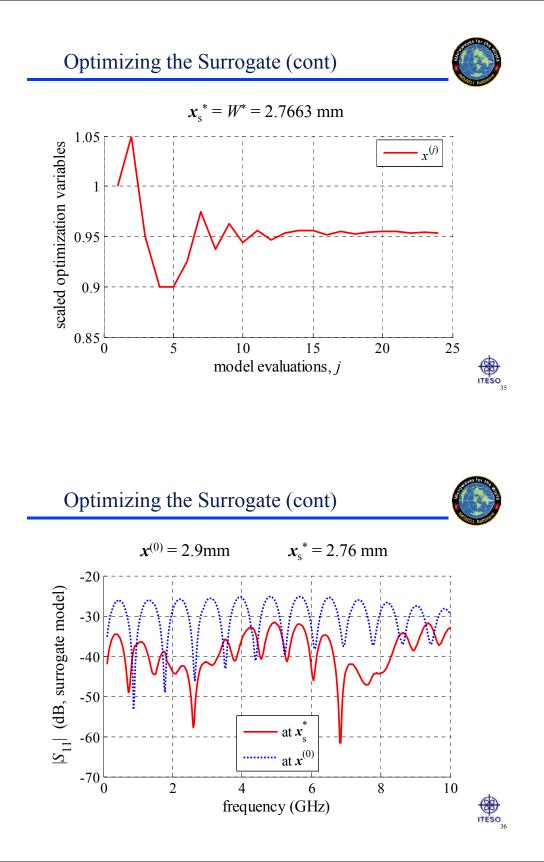


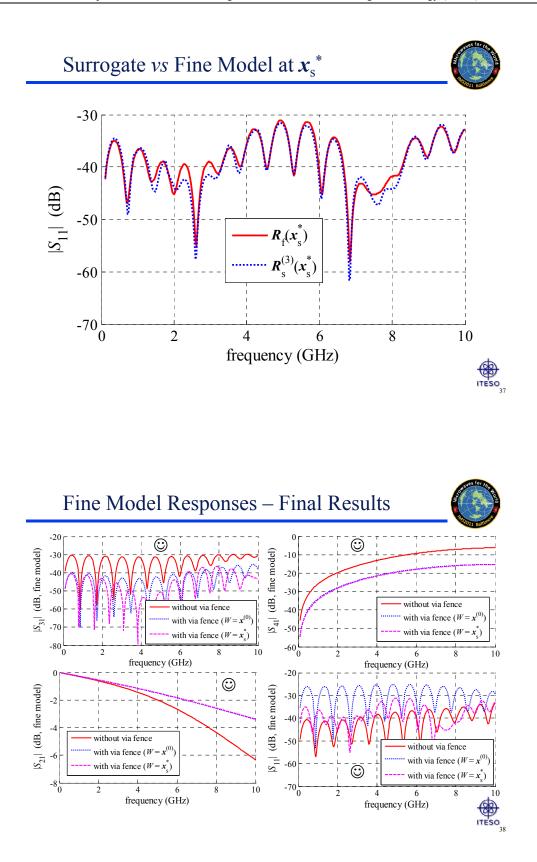
Maximum errors in learning and testing sets for the surrogate models of $|S_{11}|$











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Conclusions

- EM-based design optimization of microwave circuits using multidimensional polynomial surrogate models was described
- This formulation can be applied when no coarse model is available
- Global optimal weighting factors are obtained in closed form
- Generalization performance of polynomial interpolants was illustrated
- The design optimization of two high-speed PCB interconnect structures was presented

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